

## Linear-Phase FIR Transfer Functions

- It is impossible to design an IIR transfer function with an exact linear-phase
- It is always possible to design an FIR transfer function with an exact linear-phase response
- Consider a causal FIR transfer function  $H(z)$  of length  $N+1$ , i.e., of order  $N$ :

$$H(z) = \sum_{n=0}^N h[n] z^{-n}$$

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## Linear-Phase FIR Transfer Functions

- The above transfer function has a linear phase, if its impulse response  $h[n]$  is either **symmetric**, i.e.,

$$h[n] = h[N-n], \quad 0 \leq n \leq N$$

- or is **antisymmetric**, i.e.,

$$h[n] = -h[N-n], \quad 0 \leq n \leq N$$

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## Linear-Phase FIR Transfer Functions

- Since the length of the impulse response can be either even or odd, we can define four types of linear-phase FIR transfer functions
- For an antisymmetric FIR filter of odd length, i.e.,  $N$  even

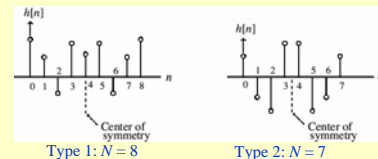
$$h[N/2] = 0$$

- We examine next the each of the 4 cases

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## Linear-Phase FIR Transfer Functions



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## Linear-Phase FIR Transfer Functions

### Type 1: Symmetric Impulse Response with Odd Length

- In this case, the degree  $N$  is even
- Assume  $N=8$  for simplicity
- The transfer function  $H(z)$  is given by

$$H(z) = h[0] + h[1]z^{-1} + h[2]z^{-2} + h[3]z^{-3} + h[4]z^{-4} + h[5]z^{-5} + h[6]z^{-6} + h[7]z^{-7} + h[8]z^{-8}$$

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## Linear-Phase FIR Transfer Functions

- Because of symmetry, we have  $h[0] = h[8]$ ,  $h[1] = h[7]$ ,  $h[2] = h[6]$ , and  $h[3] = h[5]$

- Thus, we can write

$$\begin{aligned} H(z) &= h[0](1 + z^{-8}) + h[1](z^{-1} + z^{-7}) \\ &\quad + h[2](z^{-2} + z^{-6}) + h[3](z^{-3} + z^{-5}) + h[4]z^{-4} \\ &= z^{-4} \{ h[0](z^4 + z^{-4}) + h[1](z^3 + z^{-3}) \\ &\quad + h[2](z^2 + z^{-2}) + h[3](z + z^{-1}) + h[4] \} \end{aligned}$$

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## Linear-Phase FIR Transfer Functions

- The corresponding frequency response is then given by

$$H(e^{j\omega}) = e^{-j4\omega} \{ 2h[0]\cos(4\omega) + 2h[1]\cos(3\omega) + 2h[2]\cos(2\omega) + 2h[3]\cos(\omega) + h[4] \}$$

- The quantity inside the braces is a real function of  $\omega$ , and can assume positive or negative values in the range  $0 \leq |\omega| \leq \pi$

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## Linear-Phase FIR Transfer Functions

- The phase function here is given by

$$\theta(\omega) = -4\omega + \beta$$

where  $\beta$  is either 0 or  $\pi$ , and hence, it is a linear function of  $\omega$  in the generalized sense

- The group delay is given by

$$\tau(\omega) = -\frac{d\theta(\omega)}{d\omega} = 4$$

indicating a constant group delay of 4 samples

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## Linear-Phase FIR Transfer Functions

- In the general case for Type 1 FIR filters, the frequency response is of the form

$$H(e^{j\omega}) = e^{-jN\omega/2} \tilde{H}(\omega)$$

where the **amplitude response**  $\tilde{H}(\omega)$ , also called the **zero-phase response**, is of the form

$$\tilde{H}(\omega) = h[\frac{N}{2}] + 2 \sum_{n=1}^{N/2} h[\frac{N}{2} - n] \cos(\omega n)$$

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## Linear-Phase FIR Transfer Functions

- Example - Consider

$$H_0(z) = \frac{1}{6} [1 + z^{-1} + z^{-2} + z^{-3} + z^{-4} + z^{-5} + \frac{1}{2} z^{-6}]$$

which is seen to be a slightly modified version of a length-7 moving-average FIR filter

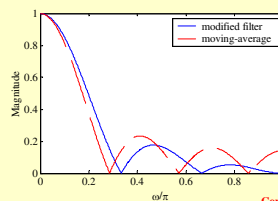
- The above transfer function has a symmetric impulse response and therefore a linear phase response

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## Linear-Phase FIR Transfer Functions

- A plot of the magnitude response of  $H_0(z)$  along with that of the 7-point moving-average filter is shown below



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## Linear-Phase FIR Transfer Functions

- Note the improved magnitude response obtained by simply changing the first and the last impulse response coefficients of a moving-average (MA) filter
- It can be shown that we can express

$$H_0(z) = \frac{1}{2}(1 + z^{-1}) \cdot \frac{1}{6}(1 + z^{-1} + z^{-2} + z^{-3} + z^{-4} + z^{-5})$$

which is seen to be a cascade of a 2-point MA filter with a 6-point MA filter

- Thus,  $H_0(z)$  has a double zero at  $z = -1$ , i.e., ( $\omega = \pi$ )

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## Linear-Phase FIR Transfer Functions

### Type 2: Symmetric Impulse Response with Even Length

- In this case, the degree  $N$  is odd
- Assume  $N = 7$  for simplicity
- The transfer function is of the form

$$H(z) = h[0] + h[1]z^{-1} + h[2]z^{-2} + h[3]z^{-3} + h[4]z^{-4} + h[5]z^{-5} + h[6]z^{-6} + h[7]z^{-7}$$

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## Linear-Phase FIR Transfer Functions

- Making use of the symmetry of the impulse response coefficients, the transfer function can be written as

$$\begin{aligned} H(z) &= h[0](1 + z^{-7}) + h[1](z^{-1} + z^{-6}) \\ &\quad + h[2](z^{-2} + z^{-5}) + h[3](z^{-3} + z^{-4}) \\ &= z^{-7/2} \{h[0](z^{7/2} + z^{-7/2}) + h[1](z^{5/2} + z^{-5/2}) \\ &\quad + h[2](z^{3/2} + z^{-3/2}) + h[3](z^{1/2} + z^{-1/2})\} \end{aligned}$$

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## Linear-Phase FIR Transfer Functions

- The corresponding frequency response is given by
- $$H(e^{j\omega}) = e^{-j7\omega/2} \{2h[0]\cos(\frac{7\omega}{2}) + 2h[1]\cos(\frac{5\omega}{2}) + 2h[2]\cos(\frac{3\omega}{2}) + 2h[3]\cos(\frac{\omega}{2})\}$$
- As before, the quantity inside the braces is a real function of  $\omega$ , and can assume positive or negative values in the range  $0 \leq |\omega| \leq \pi$

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## Linear-Phase FIR Transfer Functions

- Here the phase function is given by
- $$\theta(\omega) = -\frac{7}{2}\omega + \beta$$
- where again  $\beta$  is either 0 or  $\pi$
- As a result, the phase is also a linear function of  $\omega$  in the generalized sense
  - The corresponding group delay is
- $$\tau(\omega) = \frac{7}{2}$$

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indicating a group delay of  $\frac{7}{2}$  samples

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## Linear-Phase FIR Transfer Functions

- The expression for the frequency response in the general case for Type 2 FIR filters is of the form

$$H(e^{j\omega}) = e^{-jN\omega/2} \tilde{H}(\omega)$$

where the amplitude response is given by

$$\tilde{H}(\omega) = 2 \sum_{n=1}^{(N+1)/2} h[\frac{N+1}{2} - n] \cos(\omega(n - \frac{1}{2}))$$

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## Linear-Phase FIR Transfer Functions

### Type 3: Antisymmetric Impulse Response with Odd Length

- In this case, the degree  $N$  is even
- Assume  $N = 8$  for simplicity
- Applying the symmetry condition we get

$$H(z) = z^{-4} \{h[0](z^4 - z^{-4}) + h[1](z^3 - z^{-3}) + h[2](z^2 - z^{-2}) + h[3](z - z^{-1})\}$$

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## Linear-Phase FIR Transfer Functions

- The corresponding frequency response is given by

$$H(e^{j\omega}) = e^{-j4\omega} e^{j\pi/2} \{2h[0]\sin(4\omega) + 2h[1]\sin(3\omega) + 2h[2]\sin(2\omega) + 2h[3]\sin(\omega)\}$$

- It also exhibits a generalized phase response given by

$$\theta(\omega) = -4\omega + \frac{\pi}{2} + \beta$$

where  $\beta$  is either 0 or  $\pi$

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## Linear-Phase FIR Transfer Functions

- The group delay here is

$$\tau(\omega) = 4$$

indicating a constant group delay of 4 samples

- In the general case

$$H(e^{j\omega}) = j e^{-jN\omega/2} \tilde{H}(\omega)$$

where the amplitude response is of the form

$$\tilde{H}(\omega) = 2 \sum_{n=1}^{N/2} h[\frac{N}{2} - n] \sin(\omega n)$$

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## Linear-Phase FIR Transfer Functions

### Type 4: Antisymmetric Impulse Response with Even Length

- In this case, the degree  $N$  is even
- Assume  $N = 7$  for simplicity
- Applying the symmetry condition we get

$$H(z) = z^{-7/2} \{h[0](z^{7/2} - z^{-7/2}) + h[1](z^{5/2} - z^{-5/2}) + h[2](z^{3/2} - z^{-3/2}) + h[3](z^{1/2} - z^{-1/2})\}$$

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## Linear-Phase FIR Transfer Functions

- The corresponding frequency response is given by

$$H(e^{j\omega}) = e^{-j7\omega/2} e^{j\pi/2} \{2h[0]\sin(\frac{7\omega}{2}) + 2h[1]\sin(\frac{5\omega}{2}) + 2h[2]\sin(\frac{3\omega}{2}) + 2h[3]\sin(\frac{\omega}{2})\}$$

- It again exhibits a generalized phase response given by

$$\theta(\omega) = -\frac{7}{2}\omega + \frac{\pi}{2} + \beta$$

where  $\beta$  is either 0 or  $\pi$

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## Linear-Phase FIR Transfer Functions

- The group delay is constant and is given by

$$\tau(\omega) = \frac{7}{2}$$

- In the general case we have

$$H(e^{j\omega}) = j e^{-jN\omega/2} \tilde{H}(\omega)$$

where now the amplitude response is of the form

$$\tilde{H}(\omega) = 2 \sum_{n=1}^{(N+1)/2} h[\frac{N+1}{2} - n] \sin(\omega(n - \frac{1}{2}))$$

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## Linear-Phase FIR Transfer Functions

### General Form of Frequency Response

- In each of the four types of linear-phase FIR filters, the frequency response is of the form

$$H(e^{j\omega}) = e^{-jN\omega/2} e^{j\beta} \tilde{H}(\omega)$$

- The amplitude response  $\tilde{H}(\omega)$  for each of the four types of linear-phase FIR filters can become negative over certain frequency ranges, typically in the stopband

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## Linear-Phase FIR Transfer Functions

- The magnitude and phase responses of the linear-phase FIR are given by

$$|H(e^{j\omega})| = |\tilde{H}(\omega)|$$

$$\theta(\omega) = \begin{cases} -\frac{N\omega}{2} + \beta, & \text{for } \tilde{H}(\omega) \geq 0 \\ -\frac{N\omega}{2} + \beta - \pi, & \text{for } \tilde{H}(\omega) < 0 \end{cases}$$

- The group delay in each case is

$$\tau(\omega) = \frac{N}{2}$$

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## Linear-Phase FIR Transfer Functions

- Note that, even though the group delay is constant, since in general  $|H(e^{j\omega})|$  is not a constant, the output waveform is not a replica of the input waveform
- An FIR filter with a frequency response that is a real function of  $\omega$  is often called a **zero-phase filter**
- Such a filter must have a noncausal impulse response

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## Zero Locations of Linear-Phase FIR Transfer Functions

- Consider first an FIR filter with a symmetric impulse response:  $h[n] = h[N-n]$
- Its transfer function can be written as

$$H(z) = \sum_{n=0}^N h[n]z^{-n} = \sum_{n=0}^N h[N-n]z^{-n}$$

- By making a change of variable  $m = N-n$ , we can write

$$\sum_{n=0}^N h[N-n]z^{-n} = \sum_{m=0}^N h[m]z^{-N+m} = z^{-N} \sum_{m=0}^N h[m]z^m$$

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## Zero Locations of Linear-Phase FIR Transfer Functions

- But,  $\sum_{m=0}^N h[m]z^m = H(z^{-1})$
- Hence for an FIR filter with a symmetric impulse response of length  $N+1$  we have  $H(z) = z^{-N}H(z^{-1})$
- A real-coefficient polynomial  $H(z)$  satisfying the above condition is called a **mirror-image polynomial (MIP)**

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## Zero Locations of Linear-Phase FIR Transfer Functions

- Now consider first an FIR filter with an antisymmetric impulse response:

$$h[n] = -h[N-n]$$

- Its transfer function can be written as

$$H(z) = \sum_{n=0}^N h[n]z^{-n} = -\sum_{n=0}^N h[N-n]z^{-n}$$

- By making a change of variable  $m = N-n$ , we get

$$-\sum_{n=0}^N h[N-n]z^{-n} = -\sum_{m=0}^N h[m]z^{-N+m} = -z^{-N}H(z^{-1})$$

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## Zero Locations of Linear-Phase FIR Transfer Functions

- Hence, the transfer function  $H(z)$  of an FIR filter with an antisymmetric impulse response satisfies the condition

$$H(z) = -z^{-N}H(z^{-1})$$

- A real-coefficient polynomial  $H(z)$  satisfying the above condition is called a **antimirror-image polynomial (AIP)**

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## Zero Locations of Linear-Phase FIR Transfer Functions

- It follows from the relation  $H(z) = \pm z^{-N} H(z^{-1})$  that if  $z = \xi_o$  is a zero of  $H(z)$ , so is  $z = 1/\xi_o$
- Moreover, for an FIR filter with a real impulse response, the zeros of  $H(z)$  occur in complex conjugate pairs
- Hence, a zero at  $z = \xi_o$  is associated with a zero at  $z = \xi_o^*$

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## Zero Locations of Linear-Phase FIR Transfer Functions

- Thus, a complex zero that is not on the unit circle is associated with a set of 4 zeros given by

$$z = re^{\pm j\phi}, \quad z = \frac{1}{r}e^{\pm j\phi}$$

- A zero on the unit circle appear as a pair

$$z = e^{\pm j\phi}$$

as its reciprocal is also its complex conjugate

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## Zero Locations of Linear-Phase FIR Transfer Functions

- Since a zero at  $z = \pm 1$  is its own reciprocal, it can appear only singly
- Now a Type 2 FIR filter satisfies  $H(z) = z^{-N} H(z^{-1})$  with degree  $N$  odd
- Hence  $H(-1) = (-1)^{-N} H(-1) = -H(-1)$  implying  $H(-1) = 0$ , i.e.,  $H(z)$  must have a zero at  $z = -1$

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## Zero Locations of Linear-Phase FIR Transfer Functions

- Likewise, a Type 3 or 4 FIR filter satisfies

$$H(z) = -z^{-N} H(z^{-1})$$

- Thus  $H(1) = -(1)^{-N} H(1) = -H(1)$  implying that  $H(z)$  must have a zero at  $z = 1$

- On the other hand, only the Type 3 FIR filter is restricted to have a zero at  $z = -1$  since here the degree  $N$  is even and hence,

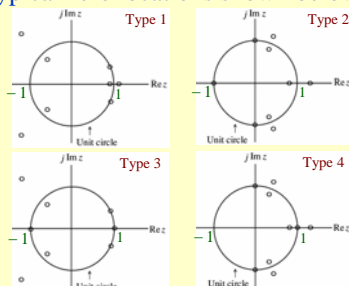
$$H(-1) = -(-1)^{-N} H(-1) = -H(-1)$$

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## Zero Locations of Linear-Phase FIR Transfer Functions

- Typical zero locations shown below



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## Zero Locations of Linear-Phase FIR Transfer Functions

- Summarizing
  - Type 1 FIR filter: Either an even number or no zeros at  $z = 1$  and  $z = -1$
  - Type 2 FIR filter: Either an even number or no zeros at  $z = 1$ , and an odd number of zeros at  $z = -1$
  - Type 3 FIR filter: An odd number of zeros at  $z = 1$  and  $z = -1$

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## Zero Locations of Linear-Phase FIR Transfer Functions

- (4) Type 4 FIR filter: An odd number of zeros at  $z = 1$ , and either an even number or no zeros at  $z = -1$
- The presence of zeros at  $z = \pm 1$  leads to the following limitations on the use of these linear-phase transfer functions for designing frequency-selective filters

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## Zero Locations of Linear-Phase FIR Transfer Functions

- A Type 2 FIR filter cannot be used to design a highpass filter since it always has a zero  $z = -1$
- A Type 3 FIR filter has zeros at both  $z = 1$  and  $z = -1$ , and hence cannot be used to design either a lowpass or a highpass or a bandstop filter

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## Zero Locations of Linear-Phase FIR Transfer Functions

- A Type 4 FIR filter is not appropriate to design a lowpass filter due to the presence of a zero at  $z = 1$
- Type 1 FIR filter has no such restrictions and can be used to design almost any type of filter

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